ECE 342 Electronic Circuits

Lecture 13 CD and CG MOS Amplifiers

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MOS Body Effect

• The threshold voltage V_T

- Depends on equilibrium potential
- Controlled by inversion in channel

The body effect

- $-V_T$ varies with bias between source and body
- Leads to modulation of V_T



Body Effect

Potential on substrate affects threshold voltage

$$V_{T}(V_{SB}) = V_{To} + \gamma \left[\left(2 \left| \phi_{F} \right| + V_{SB} \right)^{1/2} - \left(2 \left| \phi_{F} \right| \right)^{1/2} \right]$$

$$|\phi_F| = \left(\frac{kT}{q}\right) \ln\left(\frac{N_a}{n_i}\right)$$
 Fermi potential of material

$$\gamma = \frac{\left(2qN_a\varepsilon_s\right)^{1/2}}{C_{ox}}$$

Body bias coefficient

Body Effect – (Con't)

Define g_{mb} as the body transconductance

$$g_{mb} = \frac{\partial I_D}{\partial V_{BS}} \Big|_{\substack{V_{GS} = \text{constant} \\ V_{DS} = \text{constant}}}$$

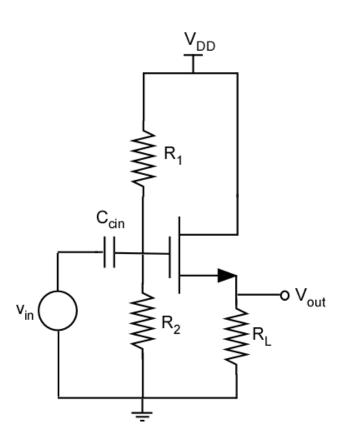
Can show that $g_{mb} = \chi g_m$

where
$$\chi = \frac{\partial V_T}{\partial V_{SB}} = \frac{\gamma}{2\sqrt{\phi_F + V_{SB}}}$$



Source Follower Configuration

For the source follower (common drain) configuration, the source is supplied at the gate and the output is collected at the source terminal.



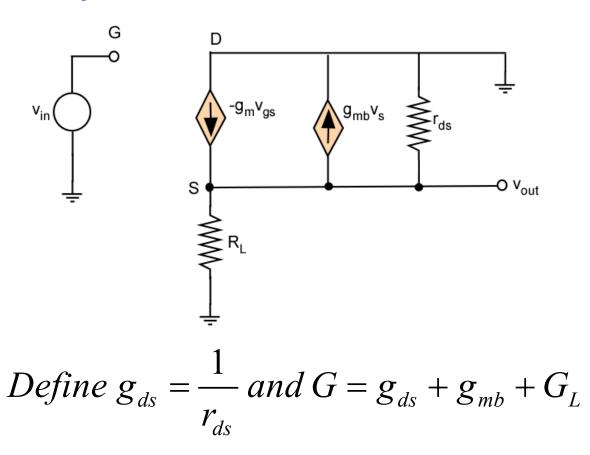
The drain terminal is connected to the power supply V_{DD} . Incrementally, the drain is grounded

The source is connected to a load resistance R_L .

Define
$$G_L = \frac{1}{R_I}$$

Source Follower Configuration

Incremental model for source follower - Since source is not tied to the substrate, we need to model the body effect. Note: substrate is always tied to ground.





$$v_{out} = \frac{g_m v_{gs}}{G} = \frac{g_m (v_{in} - v_{out})}{G}$$

$$v_{out}g_{ds} + v_{out}G_L + g_{mb}v_{out} = g_m v_{gs}$$

$$v_{out}G = g_m v_{gs} \Rightarrow v_{out} = \frac{g_m v_{gs}}{G} = \frac{g_m (v_{in} - v_{out})}{G}$$

$$v_{out}G = g_m v_{in} - g_m v_{out}$$



$$v_{out}G = g_m v_{gs} \Rightarrow v_{out}(G + g_m) = g_m v_{in}$$

$$A_{GS} = \frac{g_m}{g_m + G} = \frac{g_m}{g_m + g_{mb} + g_{ds} + G_L}$$

$$A_{GS} = \frac{g_{m}}{g_{m} + G} = \frac{g_{m}}{g_{m} + g_{mb} + g_{ds} + G_{L}}$$



Neglecting G_L and g_{ds} (since they are small)

$$A_{GS} = \frac{g_m}{g_m + g_{mb}} \approx 1$$
 This value is close to 1

Output impedance of source follower

$$R_{out} = \frac{1}{g_m} \| \frac{1}{g_{mb}} \| r_{ds} \| R_L$$

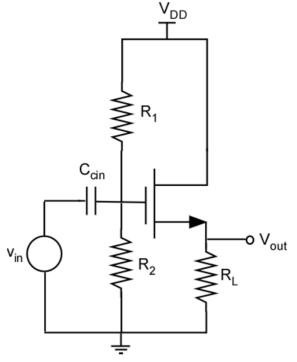
Internal output impedance

$$r_{out} = \frac{1}{g_m} \| \frac{1}{g_{mb}} \| r_{ds} \leftarrow This \ value \ is \ low$$



Source follower exhibits

- Voltage gain close to unity
- High input impedance
- Low output impedance

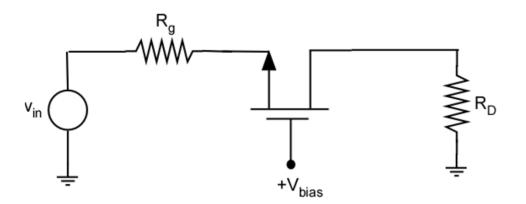


Source follower is ideal as a *Buffer* stage



Common Gate Configuration

In the common gate configuration, the signal is supplied through the source and the output is collected at the drain terminal.



The gate terminal is connected to a power supply V_{bias}. Incrementally, the gate is grounded

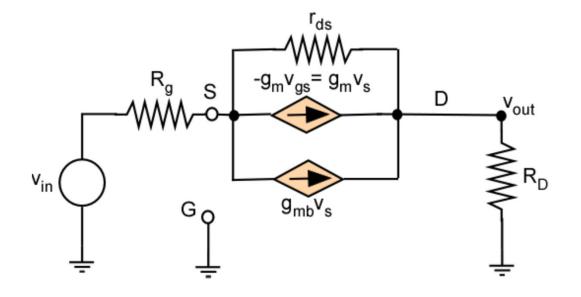
The drain is connected to a load resistance R_D.

Define
$$G_L = \frac{1}{R_L}$$



Common Gate Amplifier

Small-Signal Equivalent Circuit



Define
$$G_D = \frac{1}{R_D}$$

The midband gain is
$$A_{MB} = \frac{v_{out}}{v_{in}}$$



Common Gate Amplifier

$$A_{MB} = \frac{g_{m} + g_{mb} + g_{ds}}{G_{D} + g_{ds} + (g_{m} + g_{mb} + g_{ds})G_{D} / G_{g}}$$
$$g_{ds} \ll (g_{m} + g_{mb}) to get$$

$$A_{MB} = \frac{\left(g_m + g_{mb}\right)R_D}{1 + \left(g_m + g_{mb}\right)R_g}$$

Common Gate (CG)

- CG amplifier is non-inverting
- CG amplifier has low input impedance
- CG is unity current-gain amplifier



MOS Topologies - Ideal

	CS	CG	SF
A _{vo}	$-g_{m}R_{D}$	$g_{m}R_{D}$	1
R _{in}	∞	$\frac{1}{g_m}$	∞
R _{out}	R_{D}	R_{D}	$\frac{1}{g_m}$

