

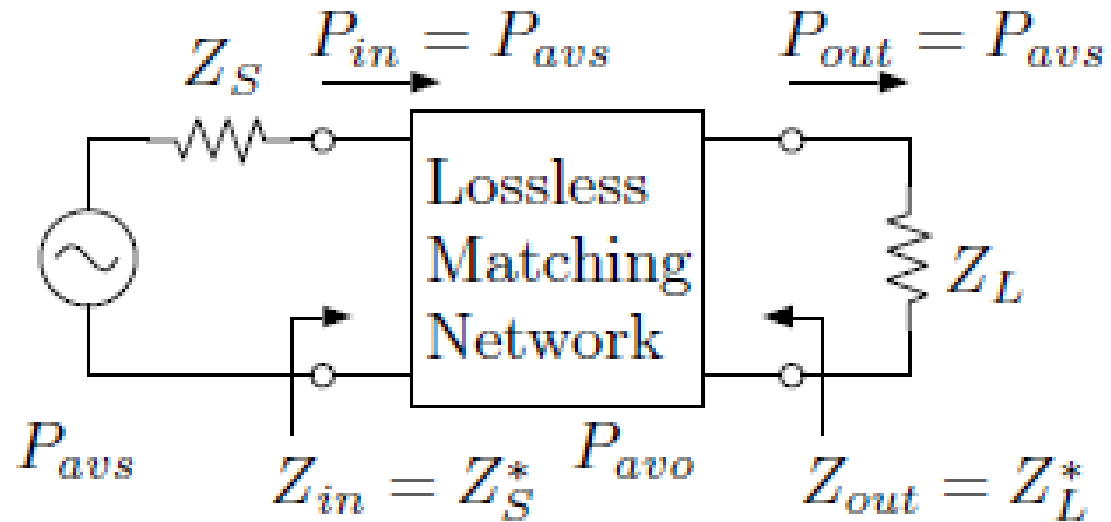
# ECE 453

# Wireless Communication Systems

## Power Definitions

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# Power Definitions



$P_{in}$ : Power delivered to input of 2-port

$P_{out}$ : Power delivered to the load

$P_{avs}$ : Power available from the source

# Power Gain Definitions

**Operating  
Power Gain**

$$G = \frac{\text{Power delivered to load}}{\text{Power delivered to input of 2-port}} = \frac{P_{out}}{P_{in}}$$

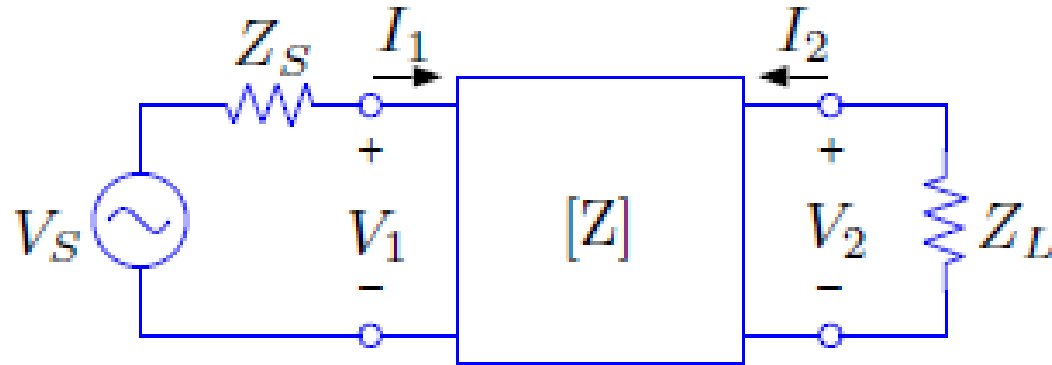
**Transducer  
Power Gain**

$$G_T = \frac{\text{Power delivered to load}}{\text{Power available from source}} = \frac{P_{out}}{P_{avs}}$$

**Available  
Power Gain**

$$G_A = \frac{\text{Power available from output}}{\text{Power available from source}} = \frac{P_{avo}}{P_{avs}}$$

# Power Available from a Source

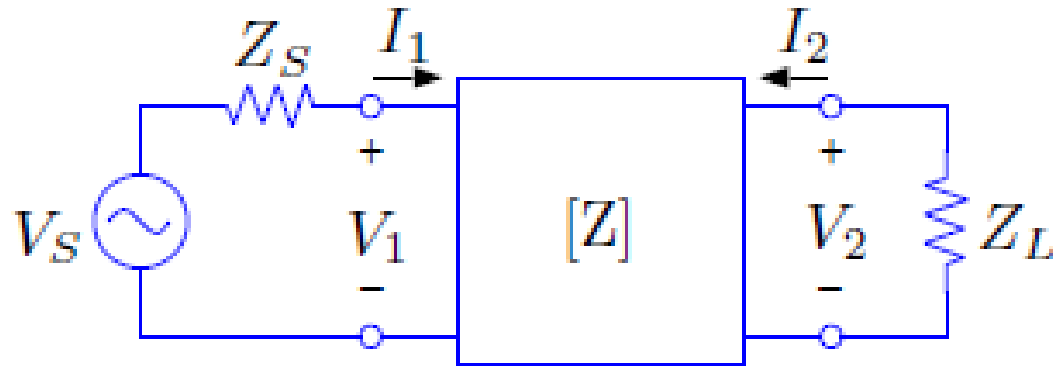


$$Z_S = R_S + jX_S$$

$$Z_L = R_L + jX_L$$

$$P_{avs} = \frac{|V_S|^2}{8R_S}$$

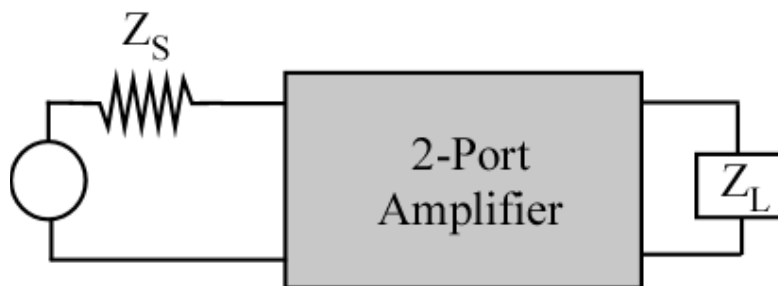
# Transducer Gain with Z-Parameters



$$G_T = 4 \frac{|Z_{21}|^2 R_L R_S}{|(Z_{11} + Z_S)(Z_{22} + Z_L) - Z_{12}Z_{21}|^2}$$

# Linear Amplifiers

The transducer power gain is defined as the power delivered to the load divided by the power available from the source.



$$\Gamma_S = \frac{Z_S - Z_o}{Z_S + Z_o}$$

$$\Gamma_L = \frac{Z_L - Z_o}{Z_L + Z_o}$$

$Z_o$  is reference impedance for S parameters

# Transducer Gain

## Definition of transducer gain

$$G_T = \frac{P_{del}}{P_{avs}}$$

## In terms of two-port scattering parameters

$$G_T = \frac{|S_{21}|^2 (1 - |\Gamma_S|^2) (1 - |\Gamma_L|^2)}{|(1 - S_{11}\Gamma_S)(1 - S_{22}\Gamma_L) - S_{21}S_{12}\Gamma_S\Gamma_L|^2}$$

# Linear Amplifiers

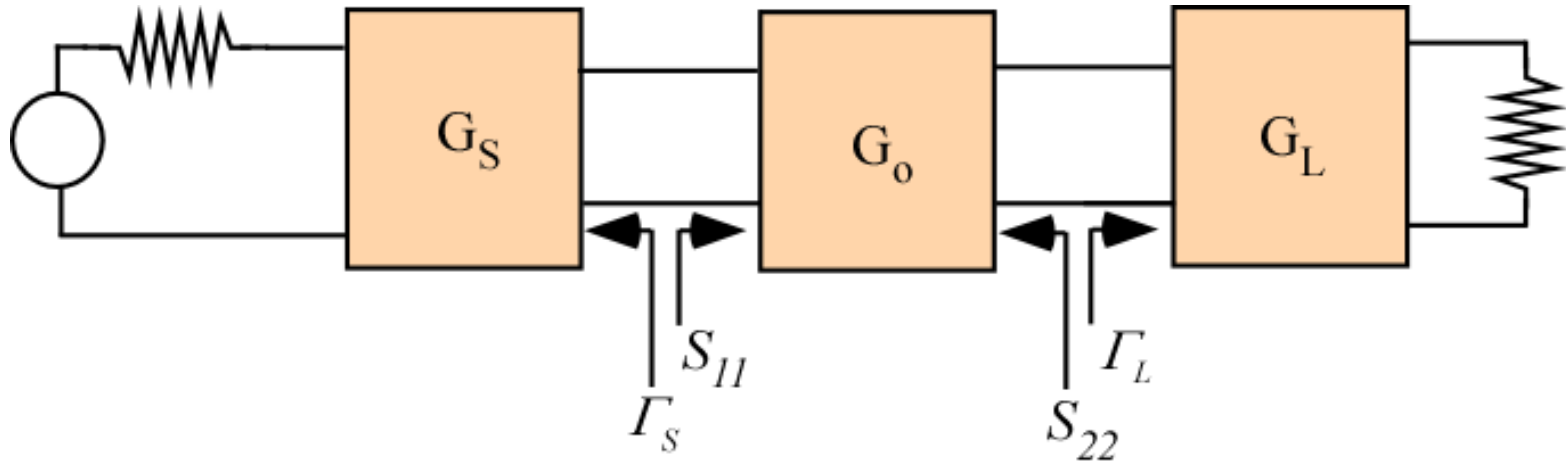
If we assume that the network is unilateral, then we can neglect  $S_{12}$  and get the unilateral transducer gain for  $S_{12}=0$ .

$$G_{TU} = |S_{21}|^2 \frac{(1 - |\Gamma_S|^2)}{|1 - S_{11}\Gamma_S|^2} \frac{(1 - |\Gamma_L|^2)}{|1 - S_{22}\Gamma_L|^2}$$

The first term ( $|S_{21}|^2$ ) depends on the transistor. The other 2 terms depend on the source and the load.

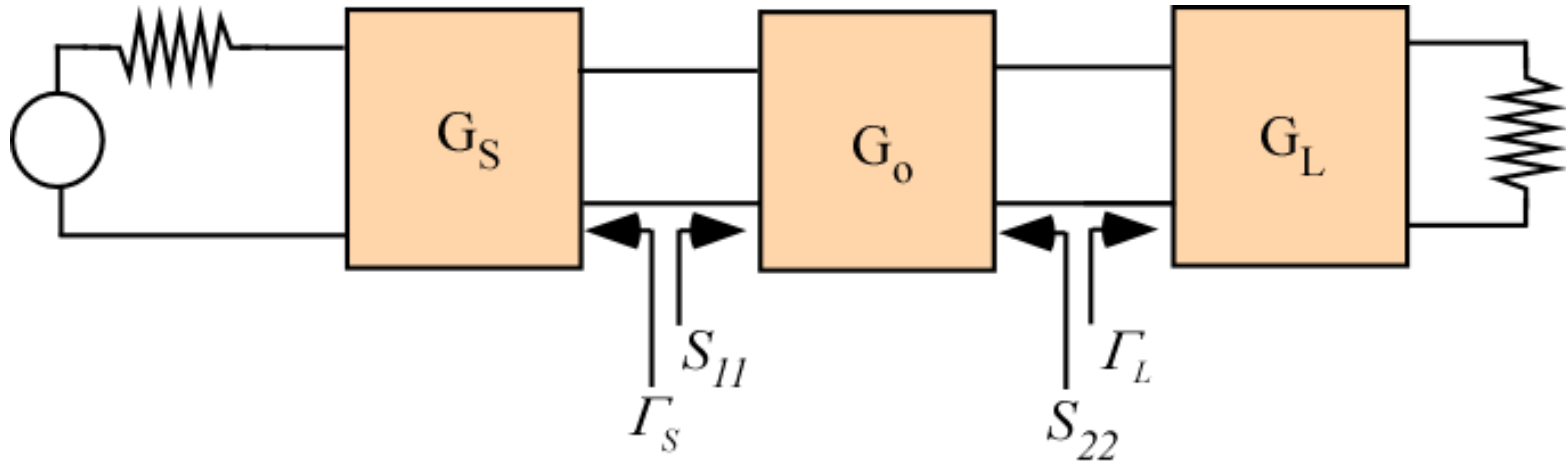


# Linear Amplifiers



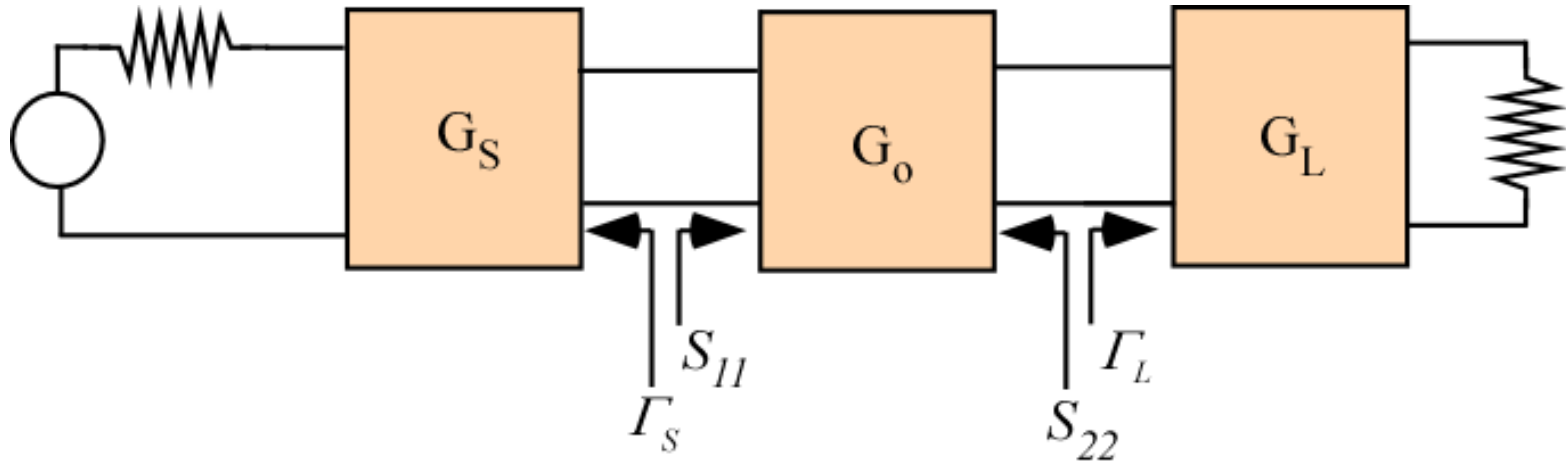
$G_S$  affects the degree of mismatch between the source and the input reflection coefficient of the two-port.

# Linear Amplifiers



$G_L$  affects the degree of mismatch between the load and the output reflection coefficient of the 2-port.

# Linear Amplifiers

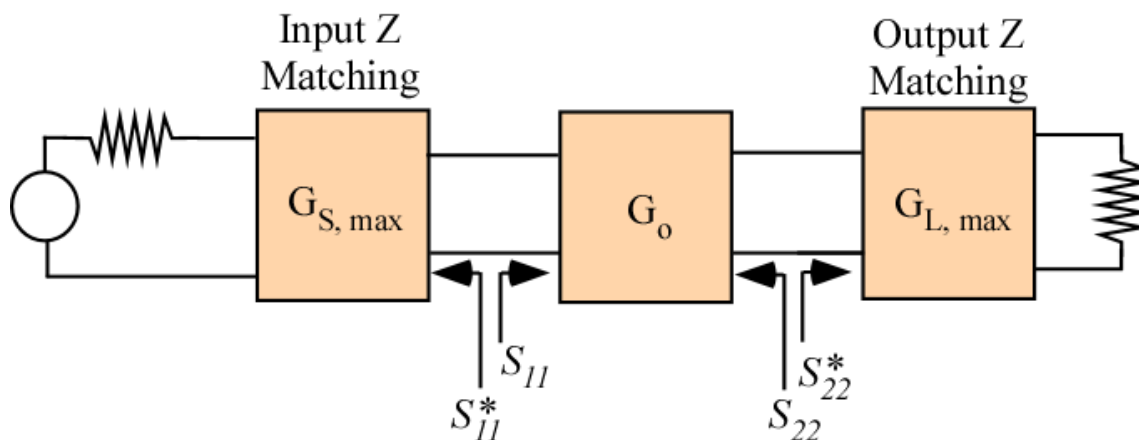


$G_o$  depends on the device and bias conditions

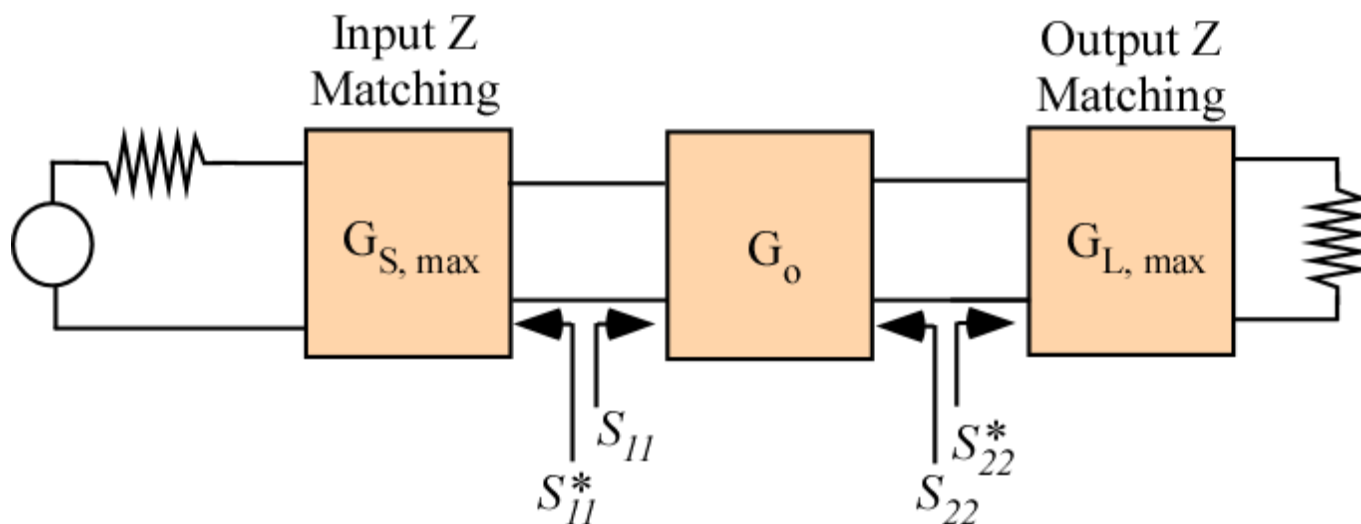
# Linear Amplifiers

Maximum unilateral transducer gain can be accomplished by choosing impedance matching networks such that.

$$\Gamma_S = S_{11}^* \qquad \Gamma_L = S_{22}^*$$
$$G_{UMAX} = \frac{1}{1 - |S_{11}|^2} \cdot |S_{21}|^2 \cdot \frac{1}{1 - |S_{22}|^2}$$



# Linear Amplifiers



$$G_{UMAX} (dB) = G_{S_{\max}} (dB) + G_o (dB) + G_{L_{\max}} (dB)$$

**For**  $\Gamma_S = S_{11}^*$ ,  **$G_S$  is a maximum**

**For**  $|\Gamma_S| = 1$ ,  **$G_S$  is 0**

# Dissipated Power

$$P_d = \frac{1}{2} \mathbf{a}^T (\mathbf{U} - \mathbf{S}^T \mathbf{S}^*) \mathbf{a}^*$$

The dissipation matrix  $\mathbf{D}$  is given by:

$$\mathbf{D} = \mathbf{U} - \mathbf{S}^T \mathbf{S}^*$$

Passivity insures that the system will always be stable provided that it is connected to another passive network

For passivity

- (1) the determinant of  $\mathbf{D}$  must be  $\geq 0$
- (2) the determinant of the principal minors must be  $\geq 0$

# Dissipated Power

When the dissipation matrix is 0, we have a lossless network →

$$\mathbf{S}^T \mathbf{S}^* = \mathbf{U}$$

The  $\mathbf{S}$  matrix is unitary.

For a lossless two-port:

$$|S_{11}|^2 + |S_{21}|^2 = 1$$

$$|S_{22}|^2 + |S_{12}|^2 = 1$$

If in addition the network is reciprocal, then

$$S_{12} = S_{21} \quad \text{and} \quad |S_{11}| = |S_{22}| = \sqrt{1 - |S_{12}|^2}$$