

ECE 546

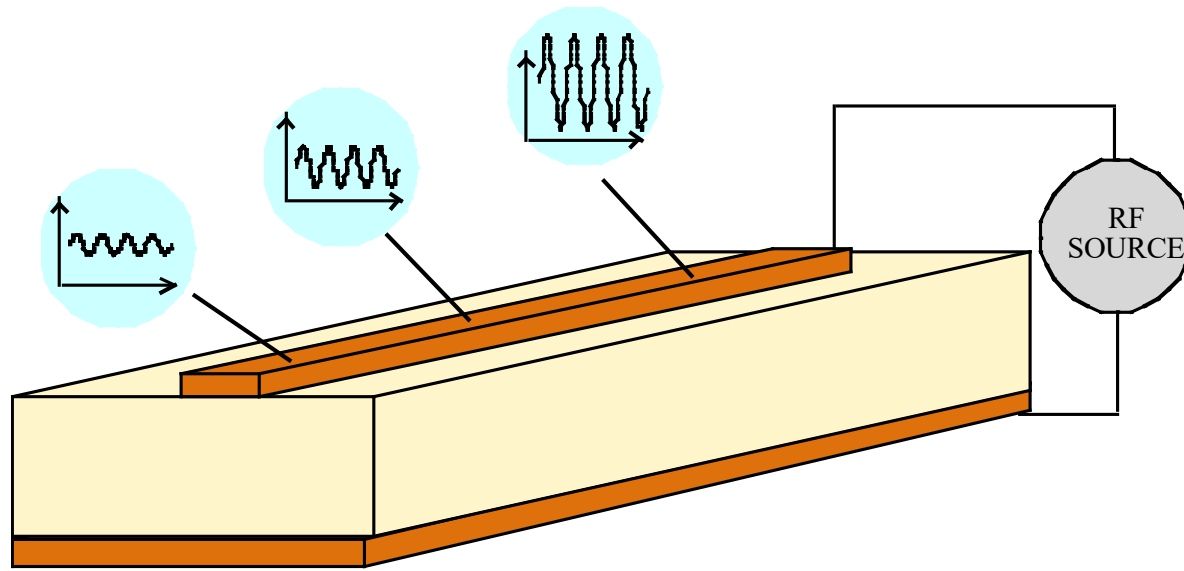
Lecture - 09

Lossy Transmission Lines

Spring 2024

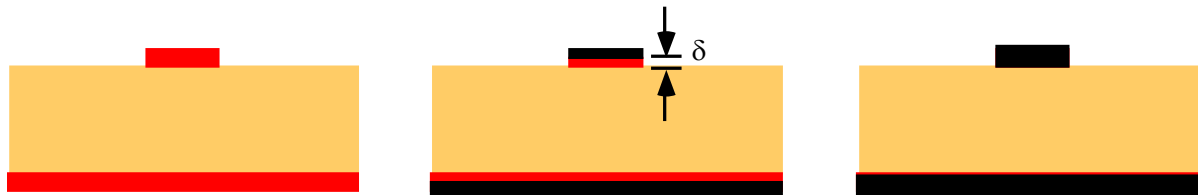
Jose E. Schutt-Aine
Electrical & Computer Engineering
University of Illinois
jesa@illinois.edu

Loss in Transmission Lines



Signal amplitude decreases with distance from the source.

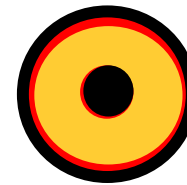
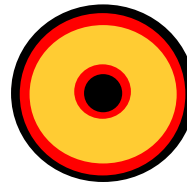
Skin Effect in Lines



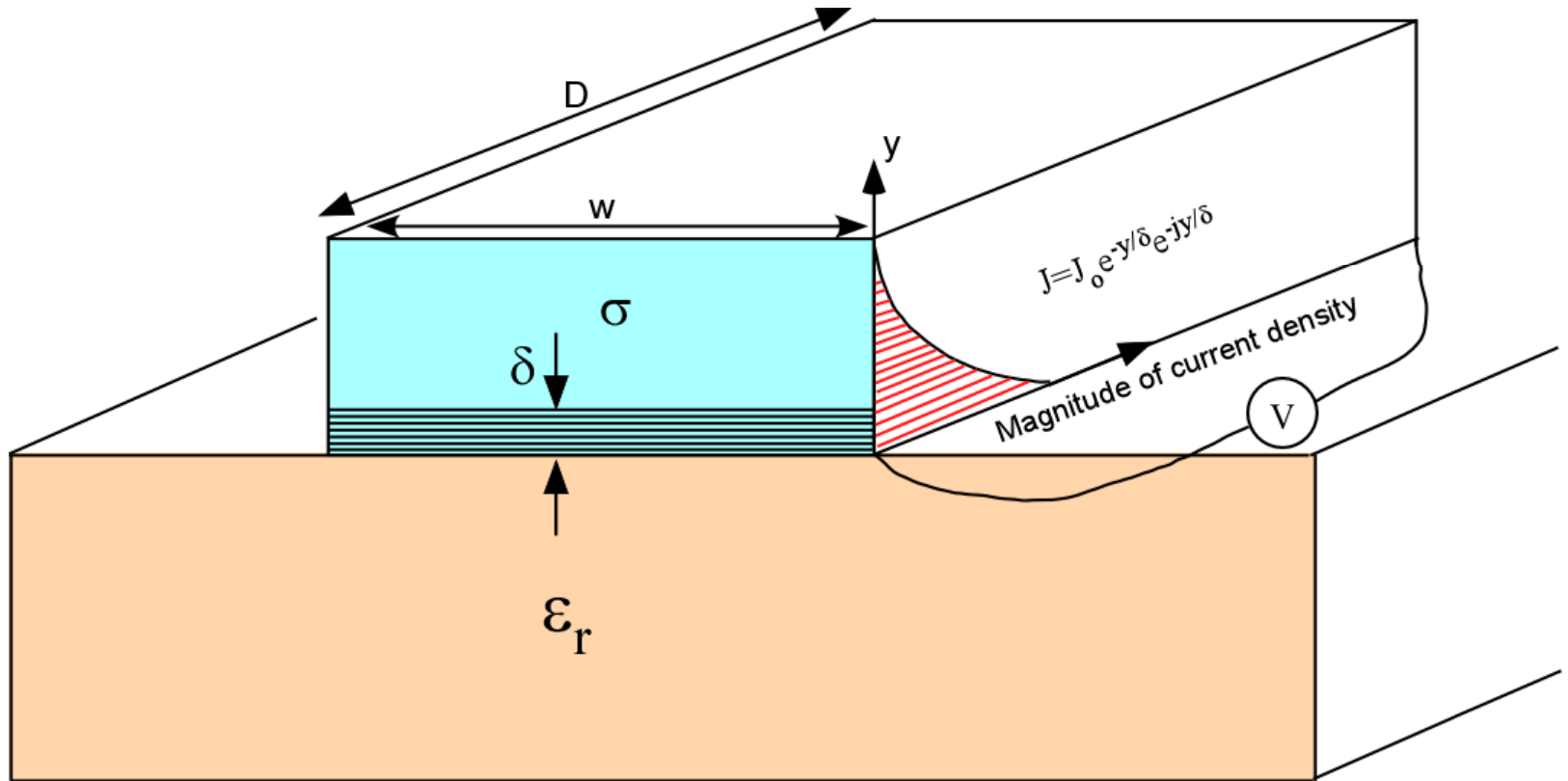
Low Frequency

High Frequency

Very High Frequency



Skin Effect in Microstrip



H. A. Wheeler, "Formulas for the skin effect," Proc. IRE, vol. 30, pp. 412-424, 1942

Skin Effect in Microstrip

Current density varies as

$$J = J_o e^{-y/\delta} e^{-jy/\delta}$$

Note that the phase of the current density varies as a function of y

$$I = \int_0^{\infty} J_o w e^{-y/\delta} e^{-jy/\delta} dy = \frac{J_o w \delta}{1 + j}$$

$$\sigma E_o = J_o \Rightarrow E_o = \frac{J_o}{\sigma}$$

The voltage measured over a section of conductor of length D is:

$$V = E_o D = \frac{J_o D}{\sigma}$$

Skin Effect in Microstrip

The skin effect impedance is

$$Z_{skin} = \frac{V}{I} = \frac{J_o D (1+j)}{\sigma J_o w \delta} = \frac{D}{w} (1+j) \sqrt{\pi f \mu \rho}$$

where $\rho = \frac{1}{\sigma}$ is the bulk resistivity of the conductor

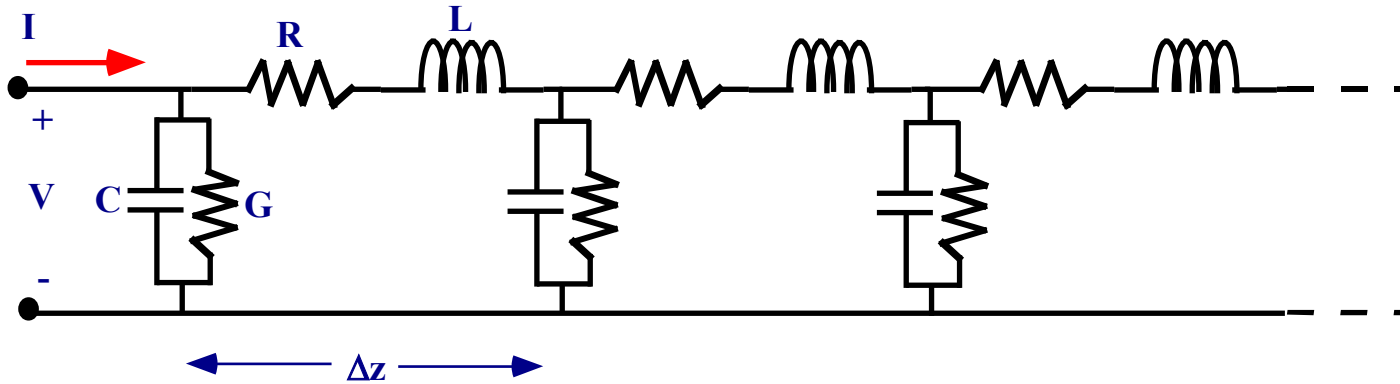
$$Z_{skin} = R_{skin} + jX_{skin}$$

with

$$R_{skin} = X_{skin} = \frac{D}{w} \sqrt{\pi f \mu \sigma}$$

➔ Skin effect has reactive (inductive) component

Lossy Transmission Line

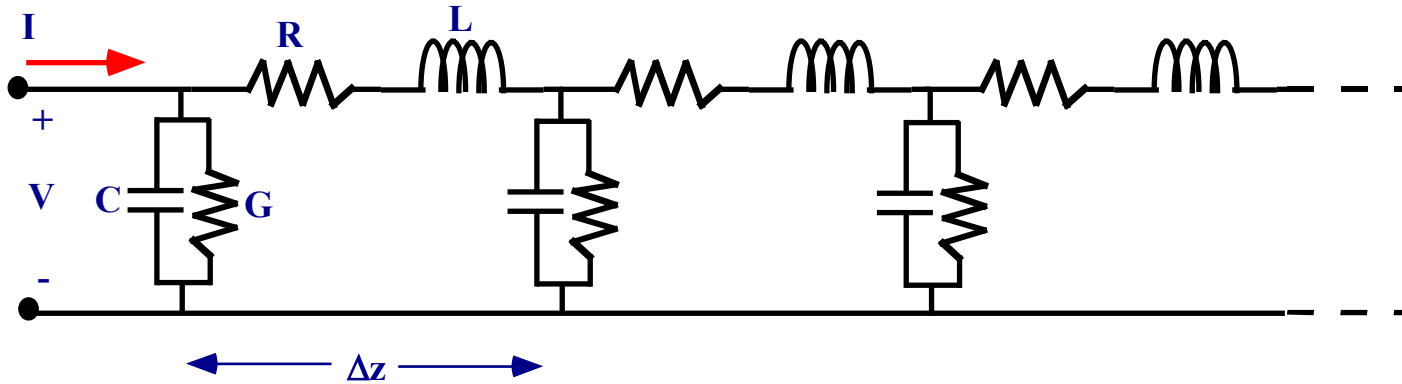


Telegraphers Equation: Time Domain

$$-\frac{\partial V}{\partial z} = RI + L \frac{\partial I}{\partial t}$$

$$-\frac{\partial I}{\partial z} = GV + C \frac{\partial V}{\partial t}$$

Lossy Transmission Line



Telegraphers Equation: Frequency Domain

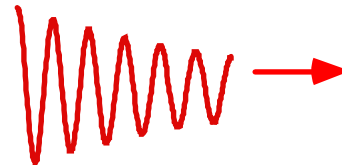
$$-\frac{\partial V}{\partial z} = (R + j\omega L)I = ZI$$

$$-\frac{\partial I}{\partial z} = (G + j\omega C)V = YV$$

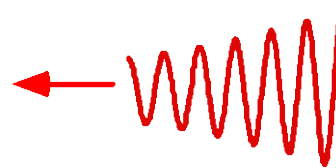
Lossy Transmission Line



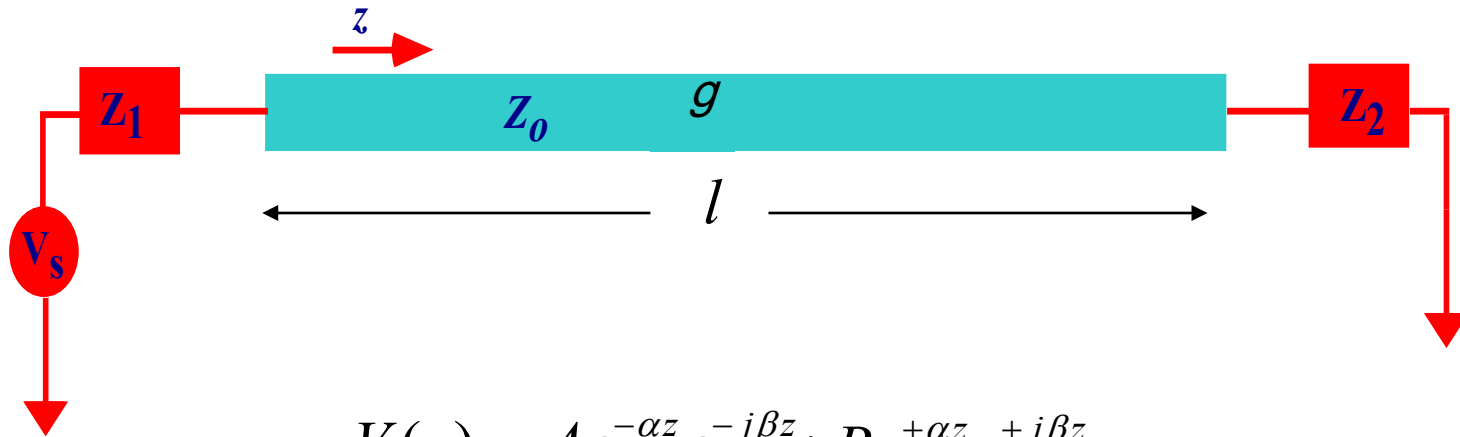
forward wave



backward wave



Lossy Transmission Line



$$V(z) = Ae^{-\alpha z} e^{-j\beta z} + Be^{+\alpha z} e^{+j\beta z}$$

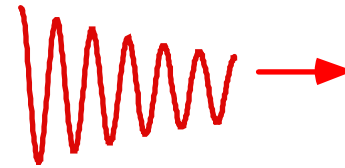
$$I(z) = \frac{1}{Z_0} \left[Ae^{-\alpha z} e^{-j\beta z} - Be^{+\alpha z} e^{+j\beta z} \right]$$

$$Z_0 = \sqrt{\frac{(R + j\omega L)}{(G + j\omega C)}}$$

$$\gamma = \alpha + j\beta = \sqrt{(R + j\omega L)(G + j\omega C)}$$

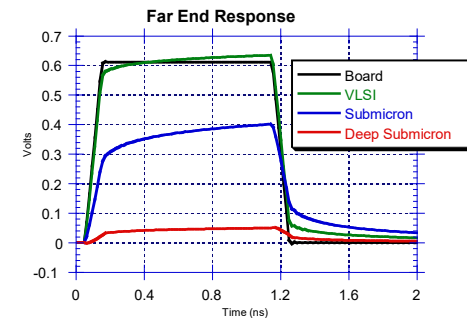
Effects of Losses

- Signal attenuation

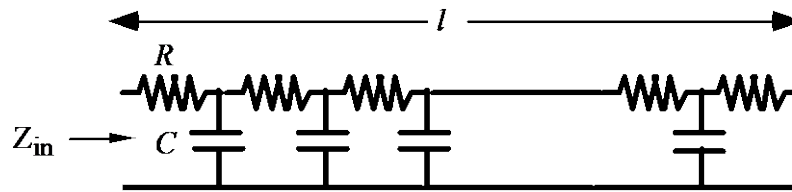


- Dispersion $\gamma = \alpha(\omega) + j\beta(\omega) = \sqrt{(R + j\omega L)(G + j\omega C)}$

- Rise time degradation



RC Transmission Line



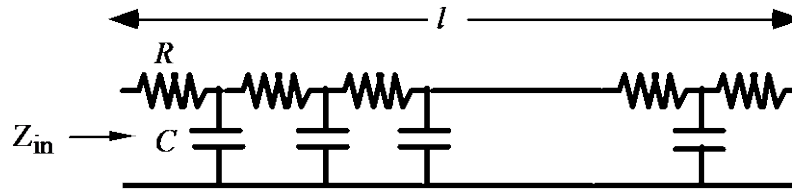
R : series resistance per unit length

C : shunt capacitance per unit length

$$Z_{in} = \frac{Rl \coth \frac{Rl}{\sqrt{2}} \sqrt{\frac{C\omega}{R}} (1+j)}{\frac{Rl}{\sqrt{2}} \sqrt{\frac{C\omega}{R}} (1+j)}$$

For very high ω , $\arg(Z_{in}) \approx 45^\circ$

RC Transmission Line



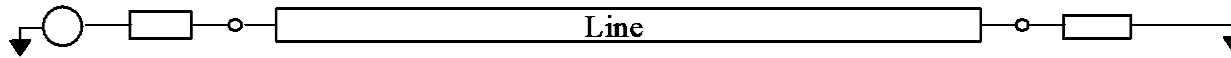
If $\omega \ll \frac{2}{RCl^2}$ then

$$Z_{in} = \frac{Rl}{2} + \frac{1}{jCl\omega} = \frac{R_T}{2} + \frac{1}{jC_T\omega}$$

$R_T = Rl$: total resistance

$C_T = Cl$: total capacitance

RC Transmission Line

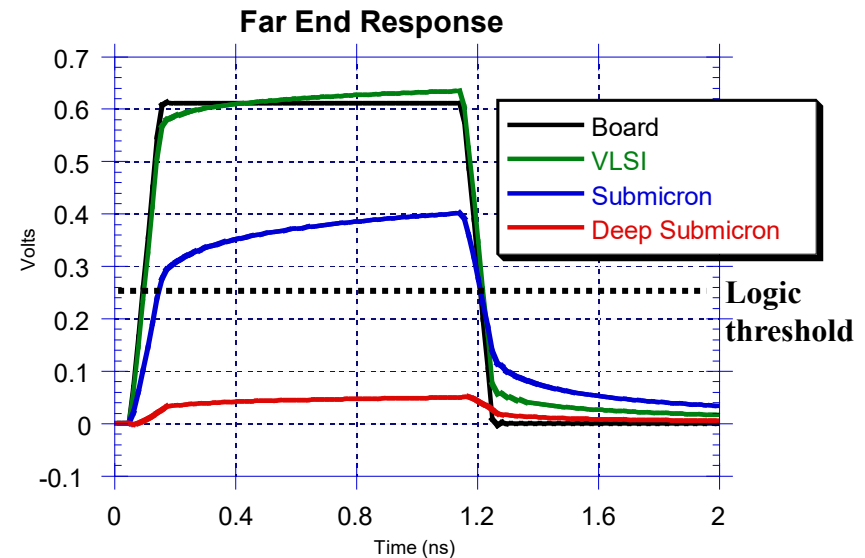
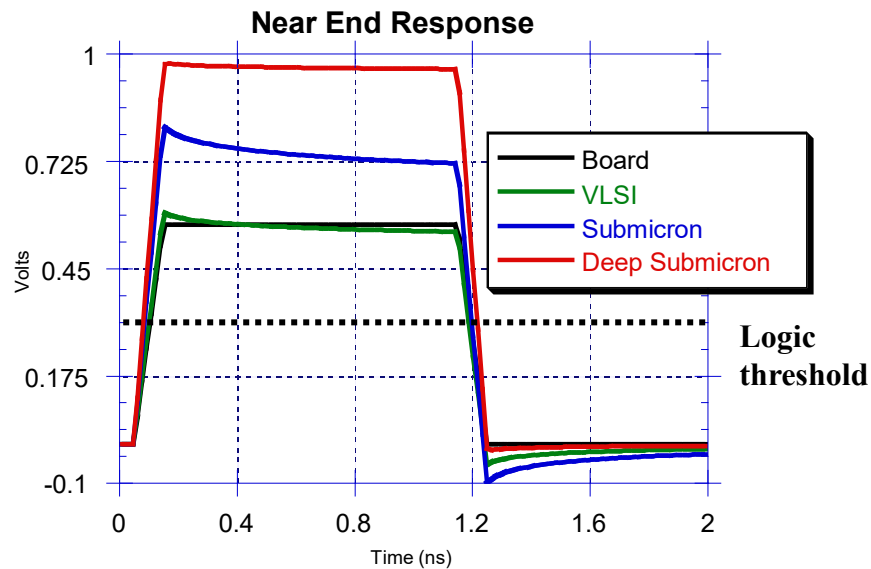


Pulse Characteristics:

rise time: 100 ps
fall time: 100 ps
pulse width: 4ns

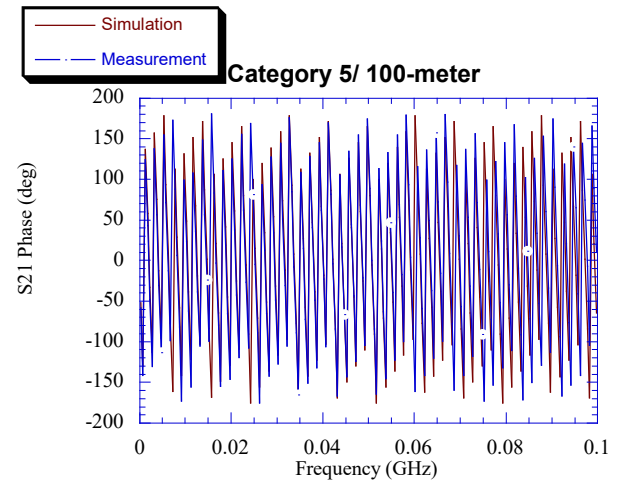
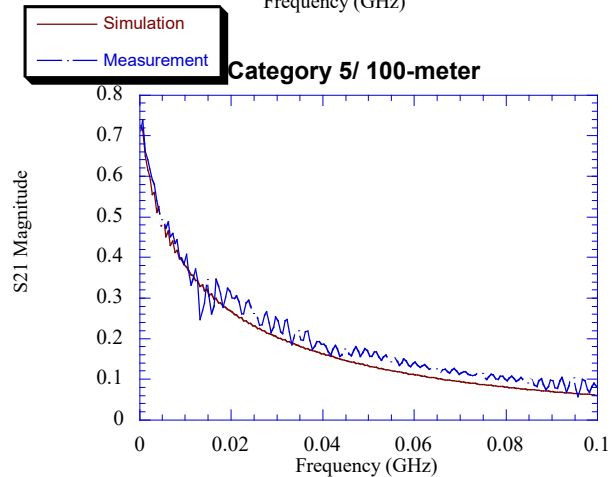
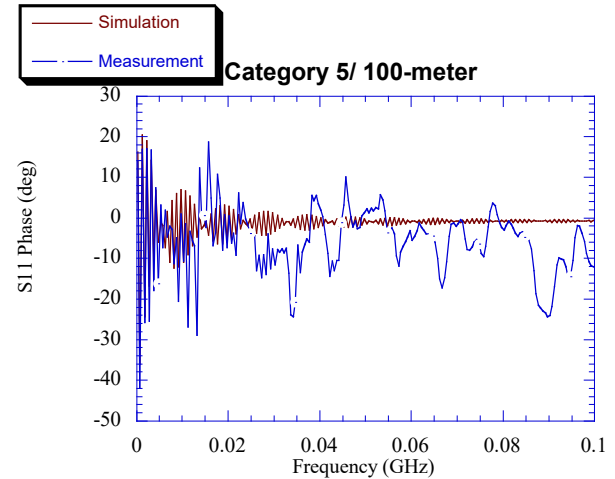
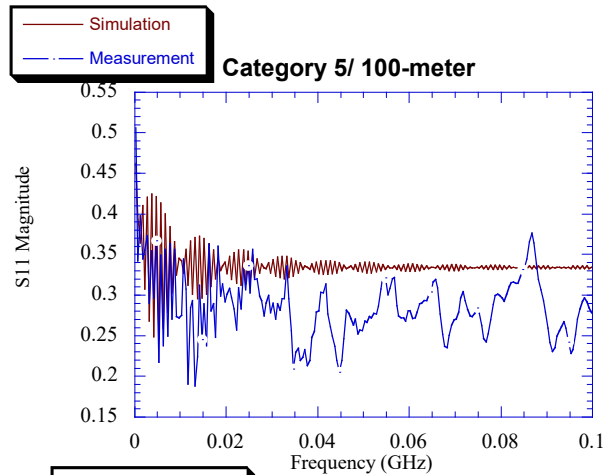
Line Characteristics

length : 3 mm
near end termination: 50 Ω
far end termination 65 Ω



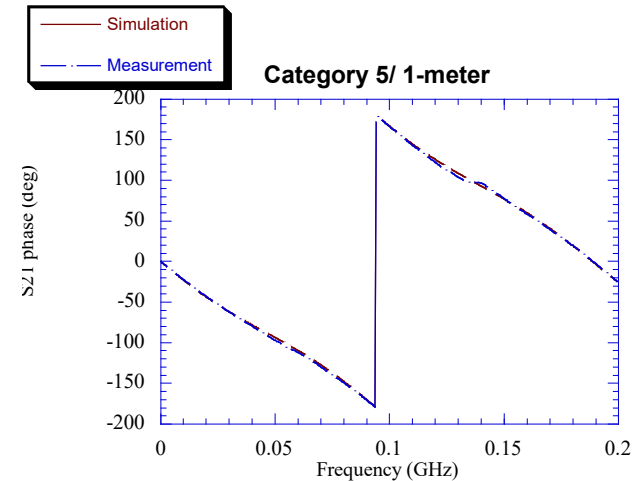
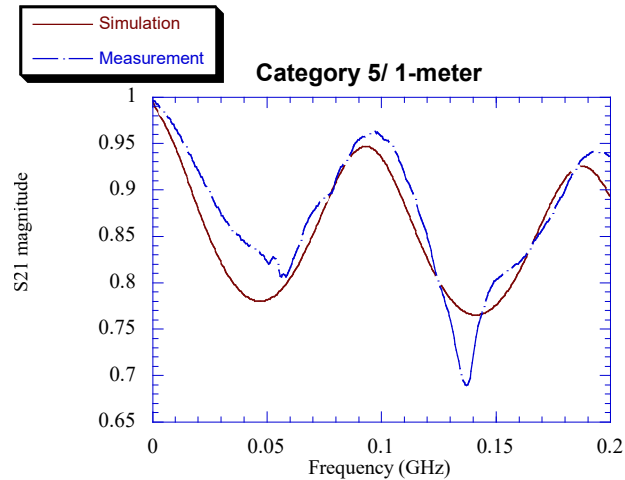
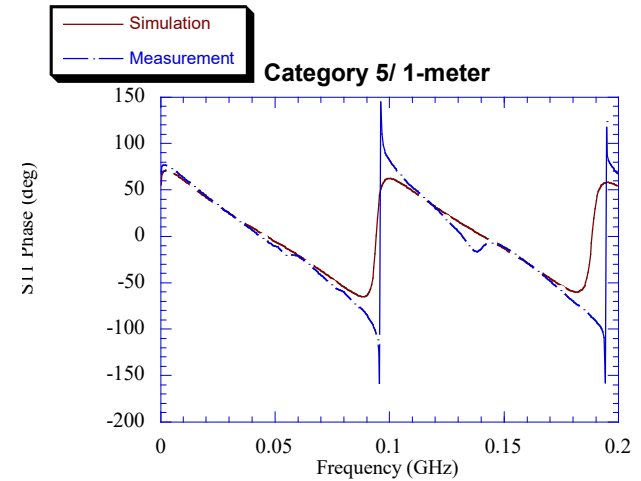
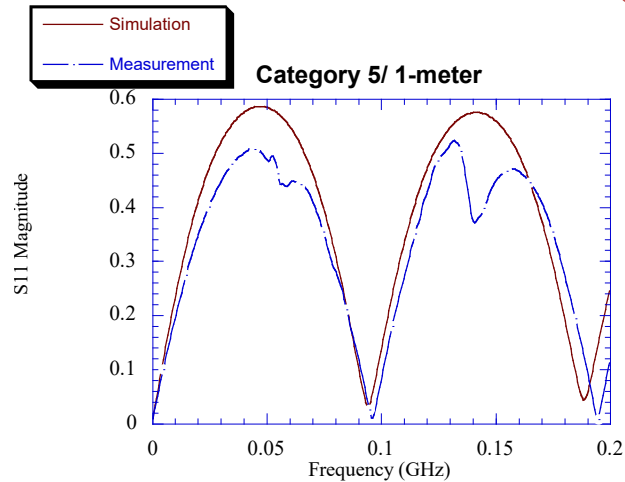
Long Cable

100m Category-5 Cable



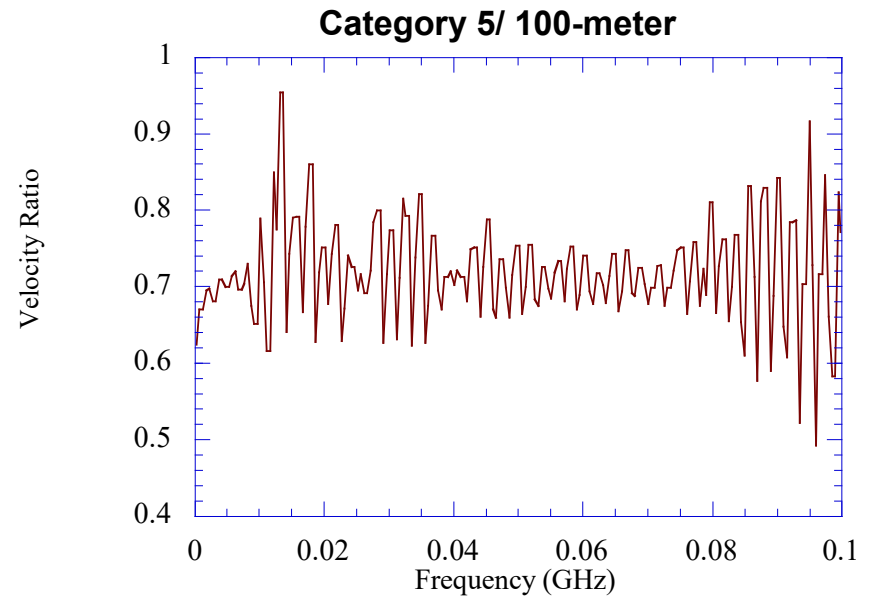
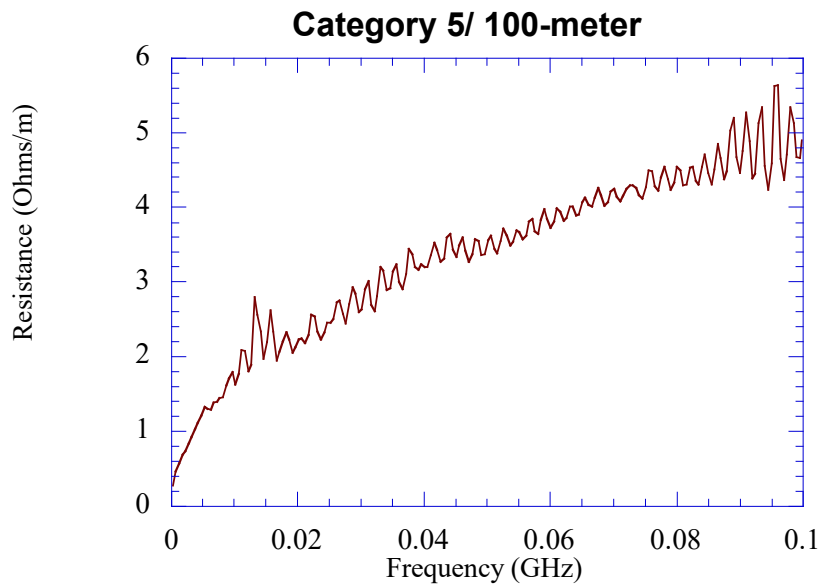
Short Cable

1m Category-5 Cable



Category 5 Cable

Resistance and velocity



Cable Loss Model

$$R(f) = R_s * f^p$$

$$v_r = v_{ro} + v_{rs} * f$$

$$Z = R(f) + j\omega L = R_{skin} + j(R_{skin} + \omega L)$$

| | $\frac{Z_0}{(\Omega)}$ | $\frac{v_{ro}}{(m/ns)}$ | $\frac{v_{rs}}{(m/ns-GHz)}$ | $\frac{R_s}{(\Omega/m-GHz^p)}$ | p | $\frac{f_{max}}{(GHz)}$ |
|-------------------|------------------------|-------------------------|-----------------------------|--------------------------------|-------|-------------------------|
| Category 5 | 100 | 0.724 | -0.165 | 15.38 | 0.482 | 0.2 |
| 24-Ga | 100 | 0.678 | 1.157 | 29.03 | 0.593 | 0.1 |
| Category 3 | 100 | 0.705 | 11.06 | 12.31 | 0.473 | 0.01 |
| SMA | 50 | 0.700 | 0.113 | 7.94 | 0.415 | 0.2 |

Lossy TL Simulation

- To simulate lossy TL with resistive loads
 - No closed form solution
 - Simplest method is to use IFFT

$$v(t, z) = IFFT \left\{ A e^{-\alpha z} e^{-j\beta z} + B e^{+\alpha z} e^{+j\beta z} \right\}$$

$$i(t, z) = IFFT \left\{ \frac{1}{Z_o} \left[A e^{-\alpha z} e^{-j\beta z} - B e^{+\alpha z} e^{+j\beta z} \right] \right\}$$

$$Z_o = \sqrt{\frac{(R + j\omega L)}{(G + j\omega C)}}$$

$$\gamma = \alpha + j\beta = \sqrt{(R + j\omega L)(G + j\omega C)}$$

$$T = \frac{Z_o}{Z_1 + Z_o}$$

$$A = \frac{TV_s(\omega)}{1 - \Gamma_1 \Gamma_2 e^{-2\gamma l}}$$

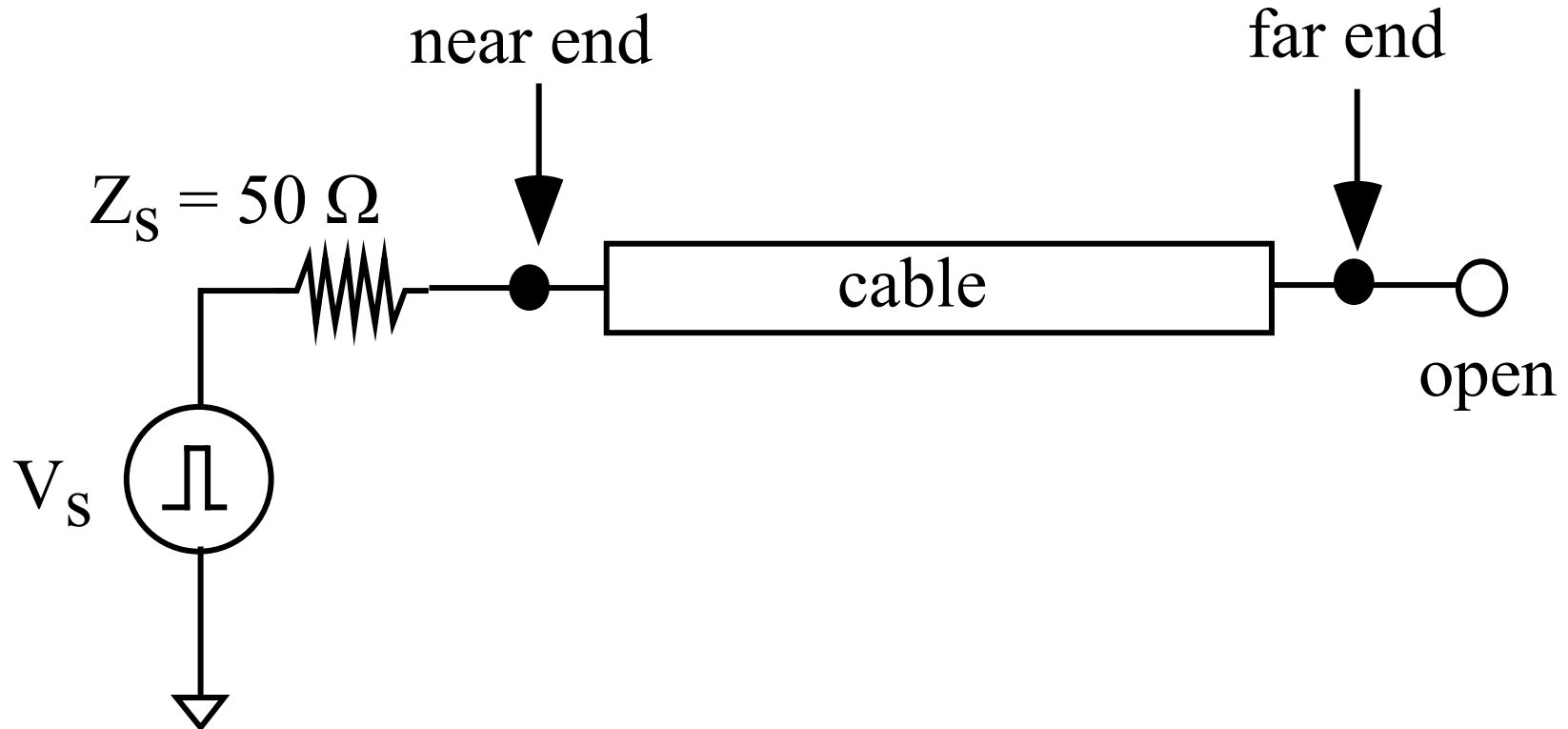
$$B = \Gamma_2 e^{-2\gamma l} A$$

$$\Gamma_2 = \frac{Z_2 - Z_o}{Z_2 + Z_o}$$

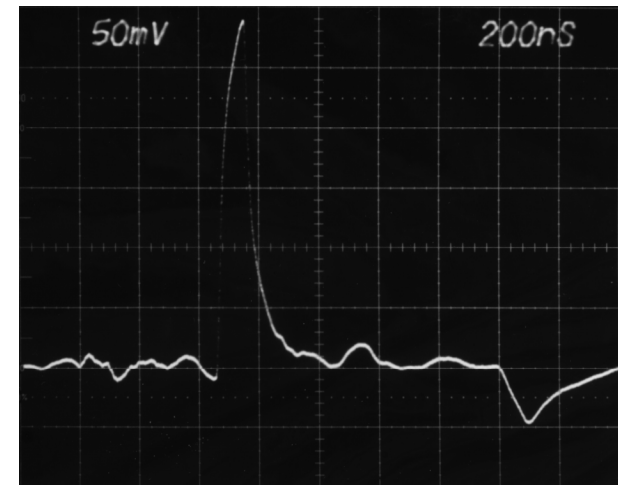
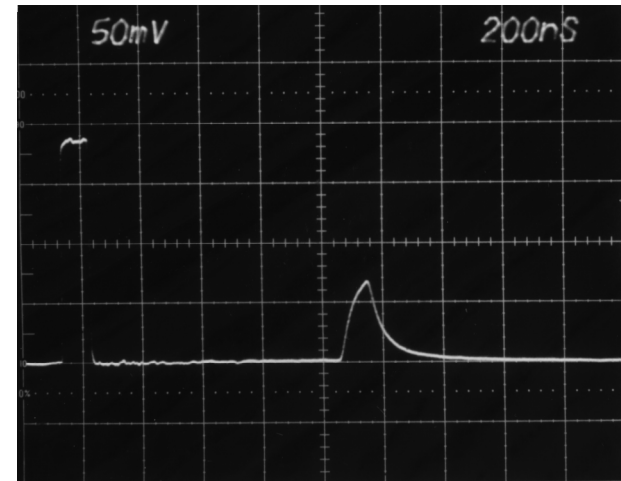
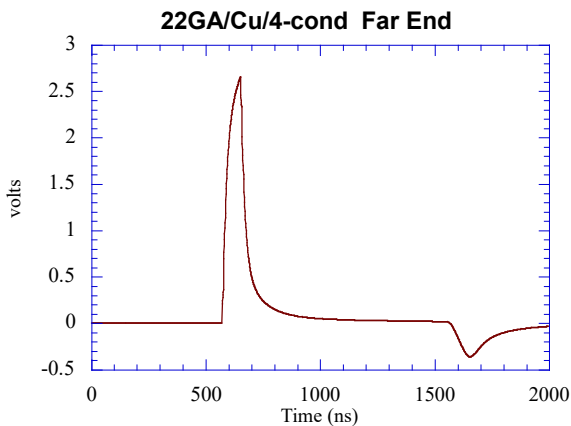
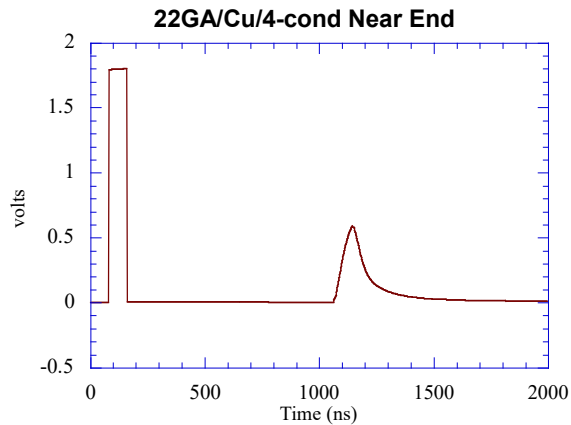
$$\Gamma_1 = \frac{Z_1 - Z_o}{Z_1 + Z_o}$$

For multiconductor transmission lines: see: J. E. Schutt-Aine and R. Mittra, "Transient analysis of coupled lossy transmission lines with nonlinear terminations," IEEE Trans. Circuit Syst., vol. CAS-36, pp. 959-967, July 1989

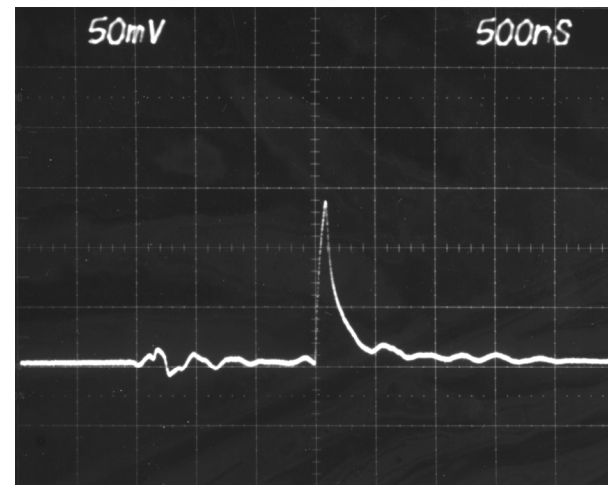
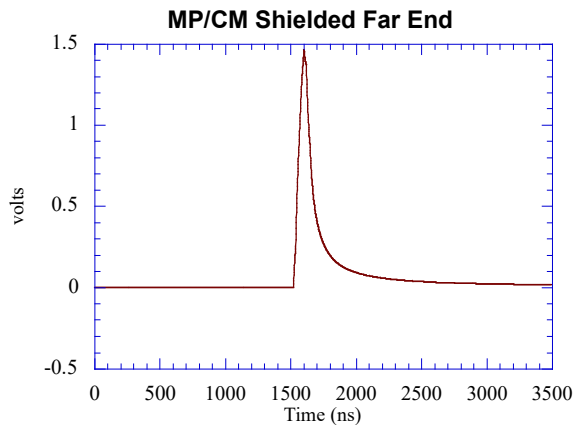
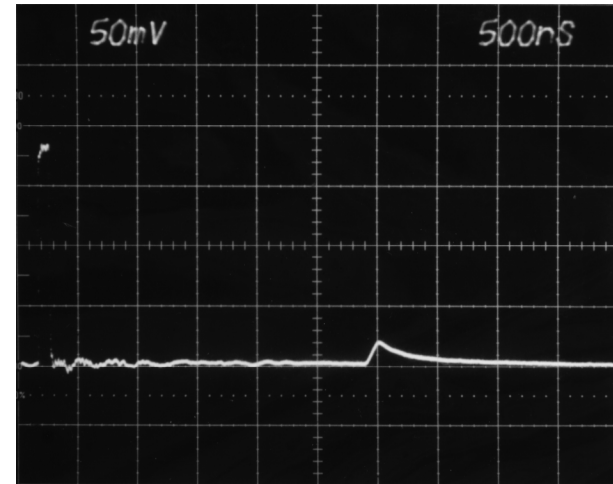
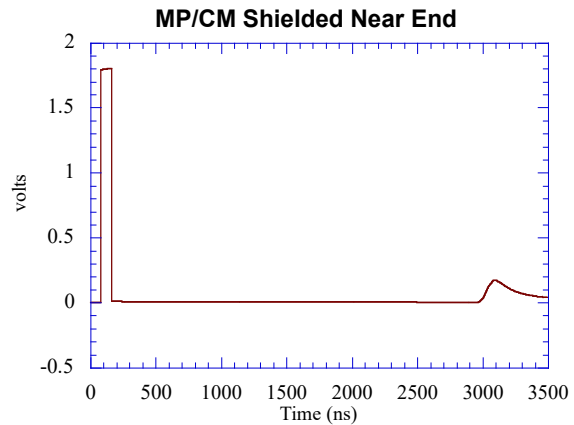
Time-Domain Simulations



Pulse Propagation (CAT-5)



Pulse Propagation (MP/CM)



Pulse Propagation (RG174)

